

Off-shore wind power generation for coastal sustainable urban development

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Outlines

- Current development of wind power generation in the world
- Potential offshore wind power generation in Hong Kong
- Development of wind turbine wake models and optimization of wind turbine layout
- Conclusions



Status of local electricity generation

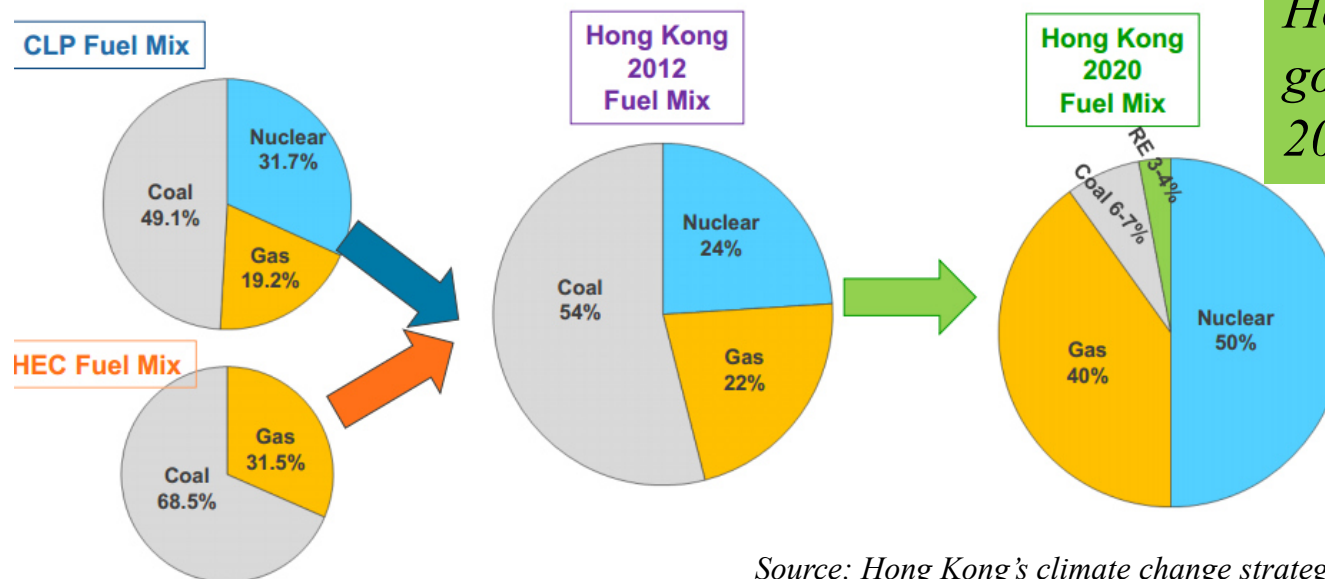
➤ In 2012, the electricity mix in Hong Kong is constituted by

✓ 24% nuclear power

✓ 22% natural gas

✓ 53% coal

✓ **0.1% renewable energy**



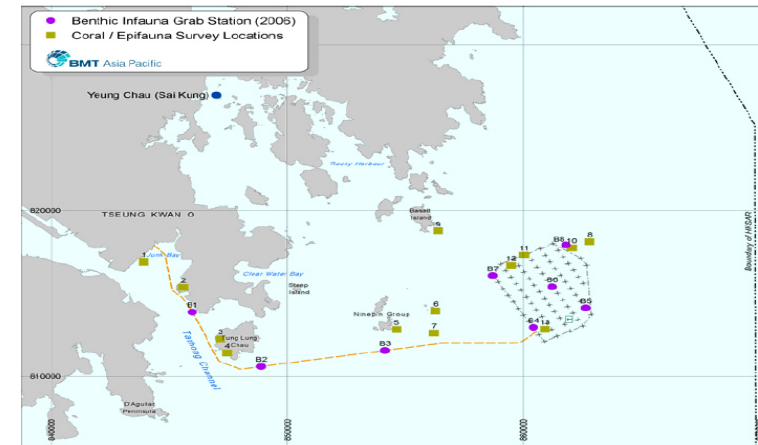
How to achieve the goal of RE 3-4% in 2020?

Source: Hong Kong's climate change strategy and action agenda
Hong Kong Energy End-use Data 2013



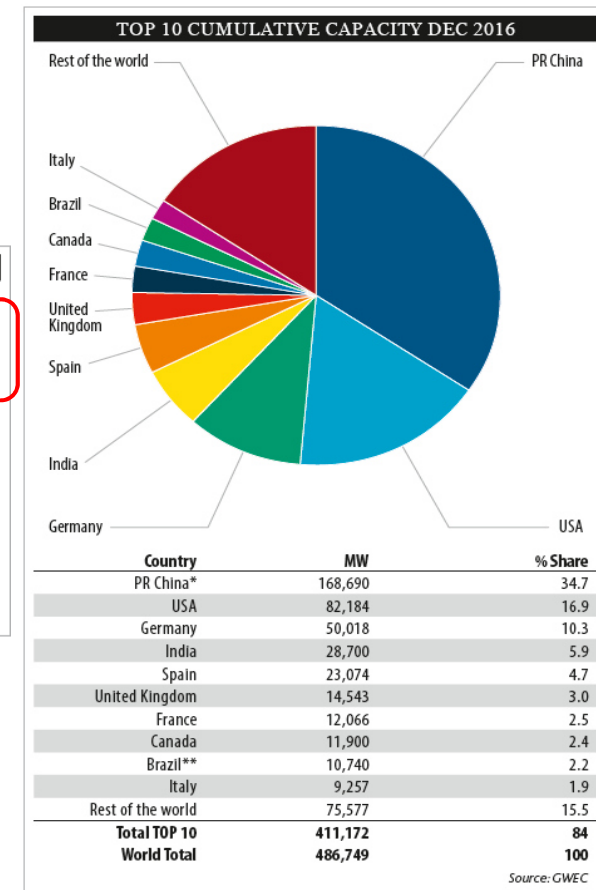
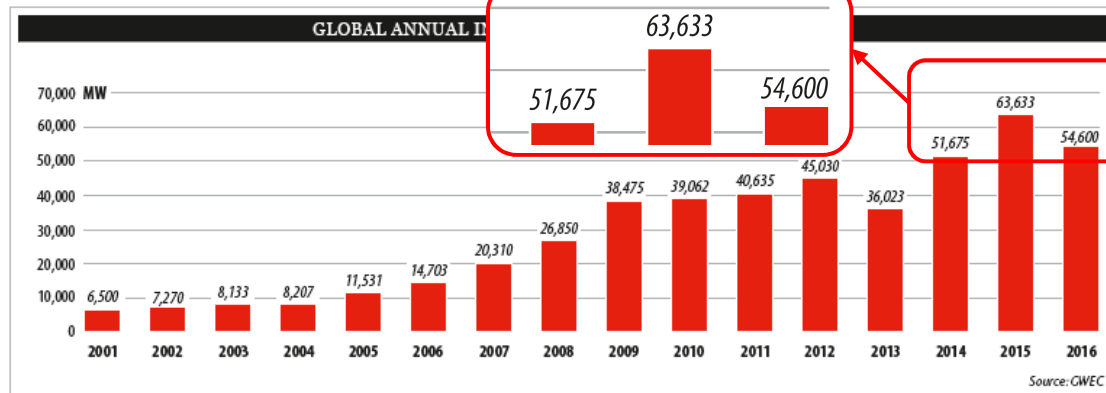
Potential renewable energy resources in Hong Kong

- Abundant solar and wind energy resources.
- 59.91% of HK area is covered by water
- **Two offshore wind farms** are proposed by CLP and HKE which are the initial attempts in offshore wind development.

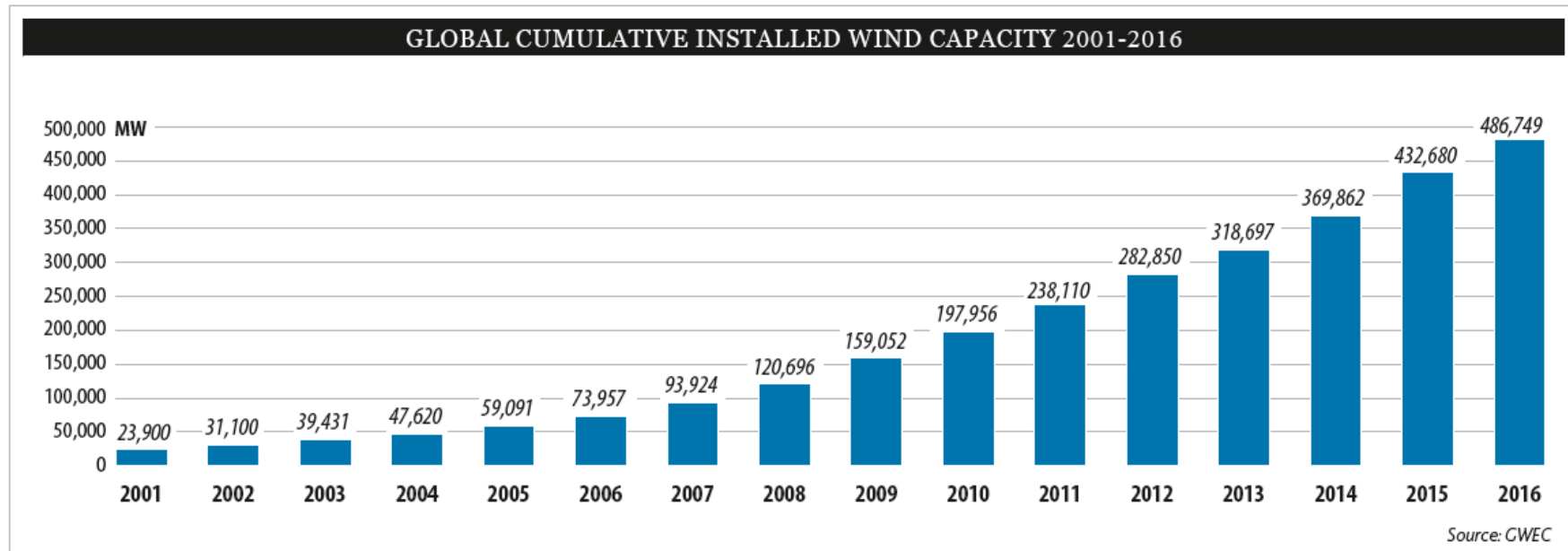


Global annual installation of wind power

◆ 2016 was a record year for the wind industry as it is the third consecutive year that annual installations crossed the 50 GW. The new global total for wind power at the end of 2016 was 486.7 GW, representing cumulative market growth of more than 12.6%.



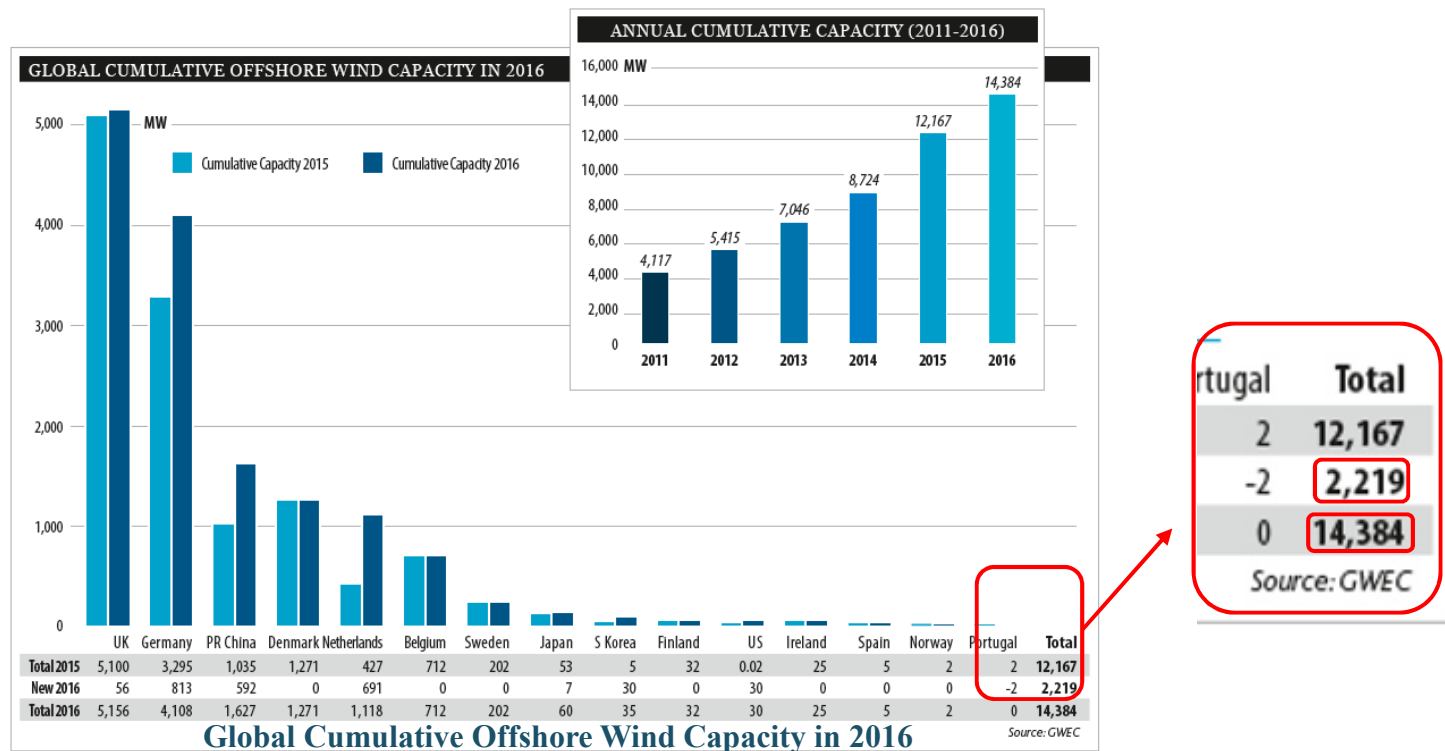
Total cumulative installation of wind power



- ◆ By the end of last year the number of countries with **more than 10,000 MW** installed capacity was **9**: including **4** in **Europe** (Germany, Spain, UK and France); **2** in **Asia-Pacific** (China & India); **2** in **North America** (US & Canada) and **1** in **Latin America** (Brazil).

Development of offshore wind power in the world

- ◆ In 2016 only, new capacity additions totaled nearly **2.2 GW** across five markets globally. This brought total offshore wind installed capacity to over **14.4 GW**.



- ◆ Annual installations of wind power in the EU have increased over the last 15 years from **3.2 GW** in 2000 to **14.4 GW** in 2016. The total offshore wind capacity is still limited, but **growth rates are very high!**

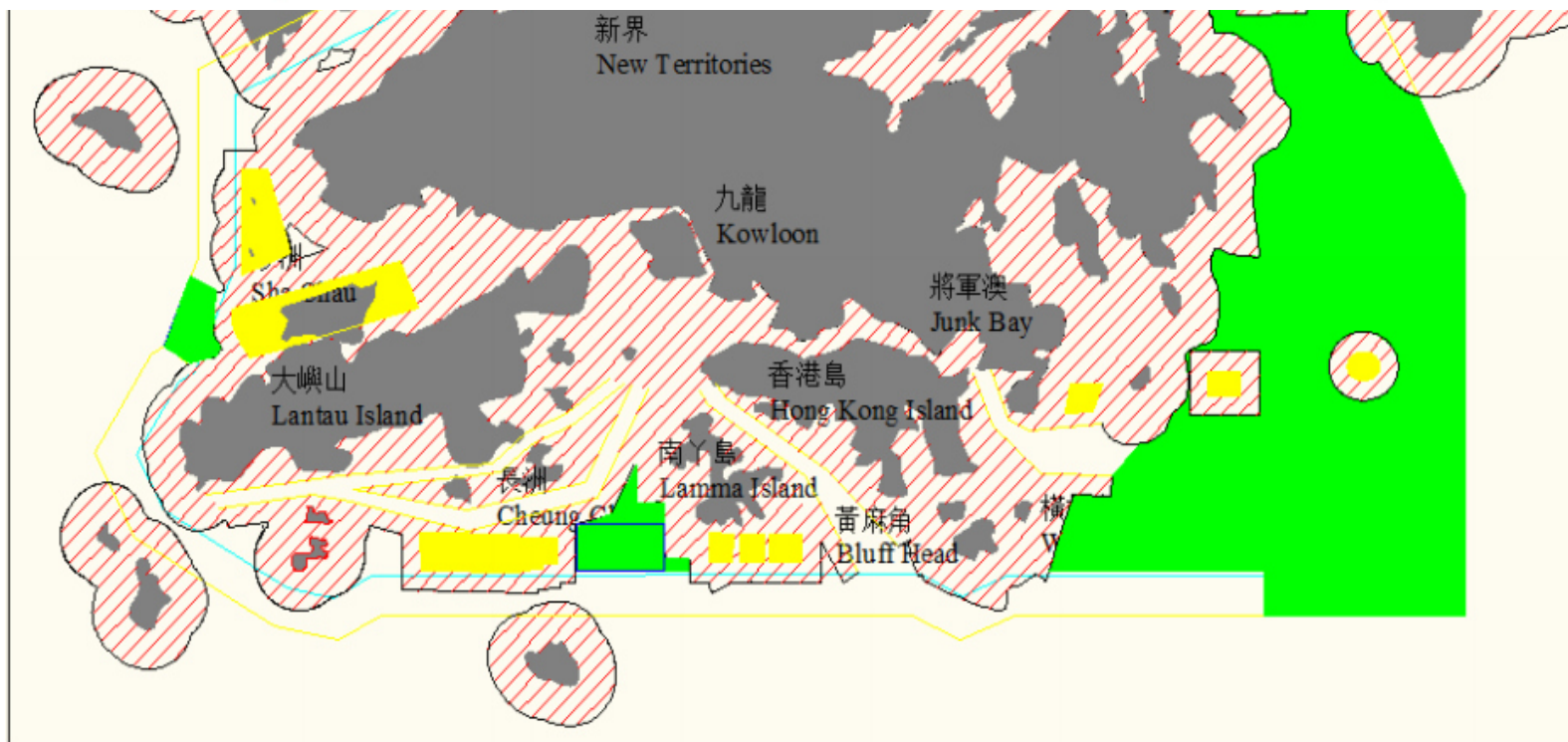


Hong Kong offshore wind power potential assessment

Offshore wind farm site selection:

The water area in Hong Kong: 1650.64 km², 59.91% of the Hong Kong territory area.

Area	Anemometer tower nearby	Potential wind farm location	Total area
2320m × 4706m	Lamma Island	Southwestern Lamma Island	16.86 km ²
Total potential offshore wind farm location area			421.48 km ²





Hong Kong offshore wind power potential assessment

Data collection from the site near Lamma island



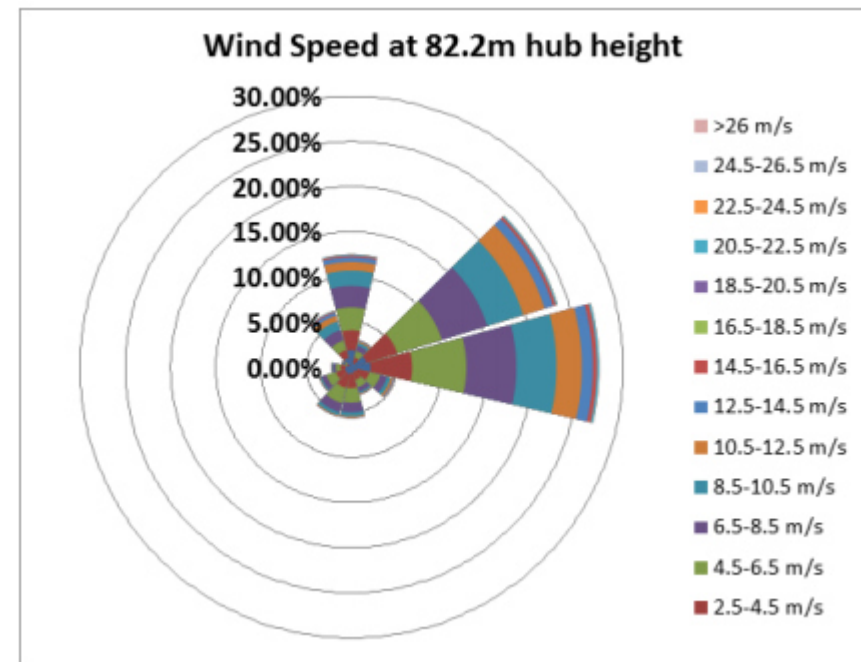
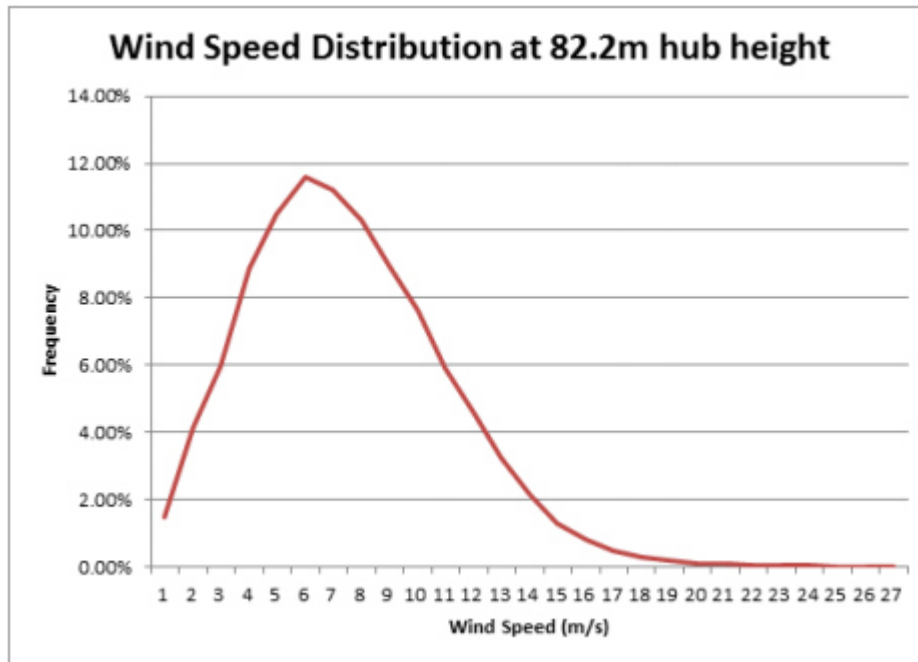


Hong Kong offshore wind power potential assessment

Input Data Source for the Selected Offshore Wind Farm

Wind in the offshore wind farm near Lamma Island

One year's wind data measured by The Hongkong Electric Co., Ltd. (HK Electric) has been used for the wind power potential analysis.





Hong Kong offshore wind power potential assessment

Wind turbine:

5 MW wind turbine is selected.

Name of parameters	Value
Hub height z (m)	85
Wind turbine rotor R_r (m)	63
Downstream rotor radius R_d (m)	77.06
Turbine thrust coefficient C_T	0.7486
Roughness length of ground z_0 (m)	0.001
The entrainment constant α	0.044
The axial induction factor a	0.249

Power generation:

$$P(v) = \begin{cases} 0; v < 3.5 \\ 5140 \times \exp(-((v - 13.31) / 5.162)^2); 3.5 \leq v < 13.31 \\ 5140; 13.31 \leq v < 30 \\ 0; v \geq 30 \end{cases}$$



Hong Kong offshore wind power potential assessment

Objective function: Lowest COE

Cost factor calculations:

Cost factor(€/MW)	Variables	Model
Turbines	Turbine size	$1.1 * 10^6$
Foundation	Water depth(h_w)	$(499h_w^2 + 6219h_w + 311810) \times 1.4 (0 < h_w < 25)$
		$(440h_w^2 + 19695h_w + 901691) \times 1.4 (h_w \geq 25)$
Grid	The least subsea cost distance d_s (km) The least land cost distance d_l (km)	$(0.38d_s + 0.4d_l + 76.6) \times 10^6 / 600$
O&M	Least cost distance to service harbour d (km)	$(0.29d^2 + 159d + 50415) \times 0.4$
Other	The percentage of investment costs	10%

COE calculations: $COE = (C_c \cdot FCR + C_{O\&M}) / AEP$

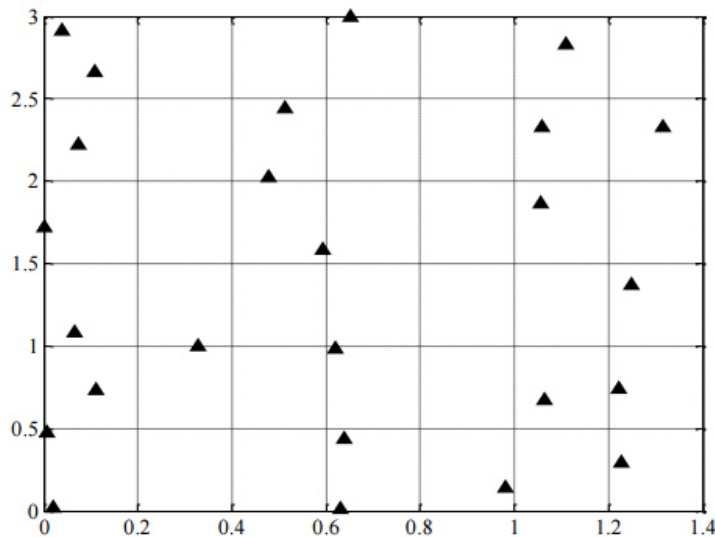
- Fixed Charge Rate = 15%
- The wind farm is operating 24 hours a day
- The price for electricity is 0.143USD/kWh = 1.45HKD/kWh



Hong Kong offshore wind power potential assessment

Optimization results of the selected wind farm near Lamma Island and the assessment of Hong Kong offshore wind power potential

Number of WTs	Total Power (10^8 kWh)	Total Cost (10^8 HKD)	COE(HKD/kWh)
25	5.78	27.24	1.55



Item	Offshore wind
Power potential	14449 GWh
Proportion of electricity use in HK in 2014	32.91%
Saving coal's importation	33374845
Proportion of importation coal	53.79%
Saving natural gas's importation	4531514
Proportion of importation natural gas	156%
COE (HKD/kWh)	~1.5



Determination of the optimal layout patterns

WF configuration	WT layout distance	APG ($\times 10^8$ kWh)	WT numbers	APG per WT ($\times 10^6$ kWh)	LCOE (HK\$/kWh)	WFE (%)
Aligned WF	14.5D \times 11.0D	5.48	28	19.56	1.474	86.84
	14.5D \times 11.5D	5.57	28	19.90	1.475	88.37
	14.5D \times 8.5D	6.58	36	18.29	1.476	81.15
	14.5D \times 9.0D	6.56	36	18.22	1.478	80.93
	14.0D \times 9.5D	6.33	32	19.78	1.480	87.85
	14.5D \times 12.0D	5.44	28	19.44	1.483	86.31
	14.5D \times 10.0D	6.39	32	19.95	1.484	88.59
	15.0D \times 12.0D	5.32	28	19.00	1.484	84.35
	14.0D \times 12.0D	5.44	28	19.43	1.489	86.25
	12.0D \times 11.5D	6.84	35	19.54	1.491	86.74
Staggered WF	14.5D \times 11.0D	5.43	28	19.39	1.467	86.07
	14.5D \times 8.5D	6.57	34	19.33	1.473	85.80
	14.0D \times 9.5D	6.33	32	19.29	1.476	85.59
	14.0D \times 11.0D	5.38	28	19.21	1.480	85.30
	14.5D \times 9.5D	6.13	32	19.16	1.485	85.08
	14.5D \times 10.0D	5.74	30	19.13	1.487	84.95
	14.5D \times 9.0D	6.50	34	19.12	1.489	84.92
	14.5D \times 11.5D	4.94	26	19.00	1.497	84.36
	15.0D \times 10.0D	5.69	30	18.97	1.500	84.23
Scattered WF	12.0D \times 11.0D	6.65	35	18.99	1.501	84.34
	-	6.29	30	20.97	1.290	93.12
	-	5.55	27	20.57	1.315	91.34
	-	5.32	26	20.48	1.321	90.94
	-	5.73	28	20.47	1.322	90.90
	-	7.84	39	20.10	1.346	89.25
	-	6.61	33	20.03	1.351	88.94
	-	6.96	35	19.88	1.361	88.28
-	4.97	25	19.86	1.362	88.19	

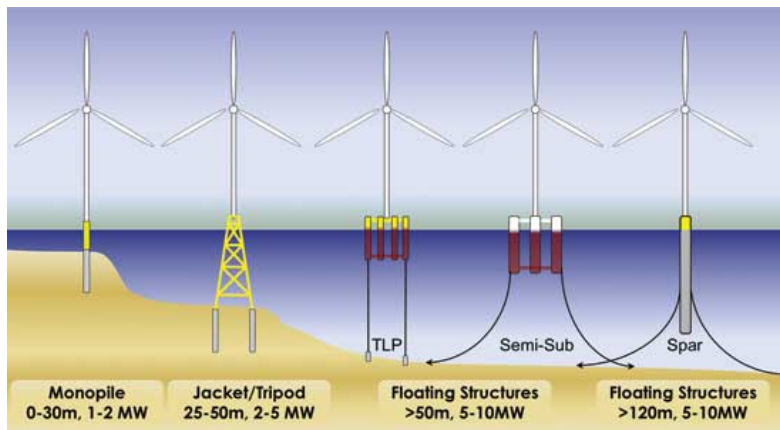
Study on Offshore Decommissioning Cost

- ◆ The year 2015 is the first time that offshore turbines were decommissioned. At one offshore wind farm of UK, the other five were installed at Sweden. In the year 2016, the decommissioned offshore wind capacity were approximately 520 MW.



First Decommissioning of an Offshore Wind Farm

- ◆ The unexpected increase in decommissioning costs is a crucial factor that cannot be ignored as for the huge economical burden.
- ◆ Some institutes estimate it will cost €200,000-500,000/MW, equals to 60-70% of installation costs (DNV GL) or 2.5% of the total project cost (The Contact Programme) to decommission offshore turbines.



Types of offshore wind turbine foundations

- ◆ The life expectancy of the offshore wind turbine is around 25–30 years. However, the foundation is always overdesigned.
- ◆ It is possible and meaningful to develop the decommissioning strategy to reduce the cost from the initial design phase of an offshore wind farm.

Decommissioning Strategy

$$Cost_{total} = Cost_{capital} + Cost_{O\&M} + Cost_{levelised}$$

Wind Turbine costs, foundation costs, installation, grid connection cost and **decommissioning cost**);

Operation and maintenance costs;

Related to wind, varies depending on the wind resource and project costs, but at good wind sites can be very competitive.

◆ Decommissioning Strategy

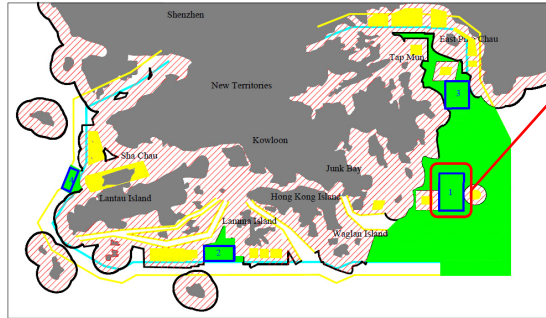
When the first generation offshore wind turbines are decommissioned, foundations can still be on service after some strengthen strategies in the second generation.

$$Cost_{capital} = Cost_{WT1} + Cost_{f1} + Cost_{install1} + Cost_{strengthen} + Cost_{WT2} + Cost_{install2} + Cost_{decommission2}$$

◆ Offshore Wind Farm Optimization

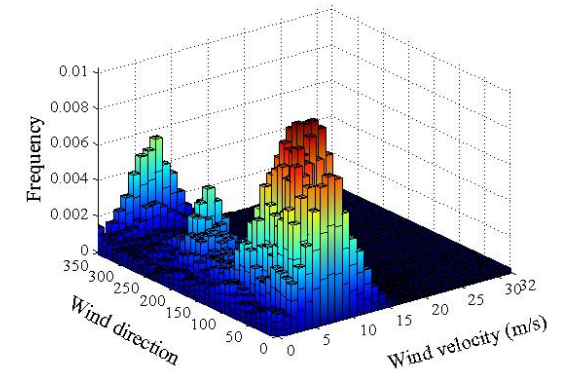
The wind turbine layout optimizing process is based on the **Multi-Population Genetic Algorithm (MPGA)**. The Cost of Energy (COE) is regarded as the criteria to judge the new method. The COE is on account of two generations' energy output and total cost.

Application of Decommissioning Strategy



Waglan Island Sea Area
Selected area: 3740m × 5828m

Wind data source:
 Royal Observatory, Hong Kong

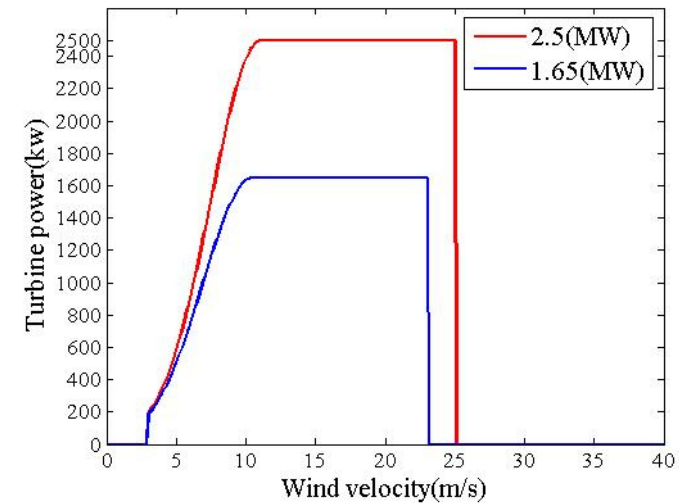


Wind Velocity Frequency Distribution in Waglan Island Sea Area

Potential Offshore Wind Farm Selections (Gao. et al)

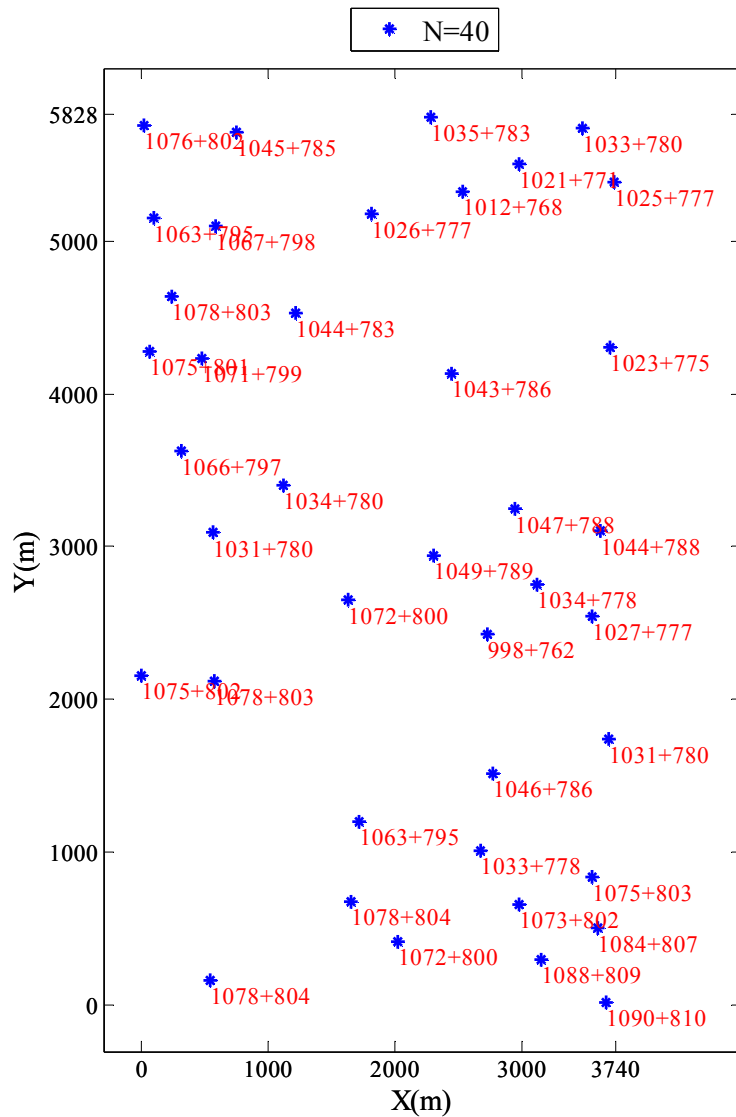
Parameters of Wind Turbines

Parameters	Turbine1	Turbine2
Rated power	2.5MW	1.65MW
Cut-in wind speed	3	3
Rated wind speed	11.1	10.5
Cut-out wind speed	25	23
Rotor diameter	108	88
Hub height	80	70



Wind Turbine Power Curves

Application of Decommissioning Strategy



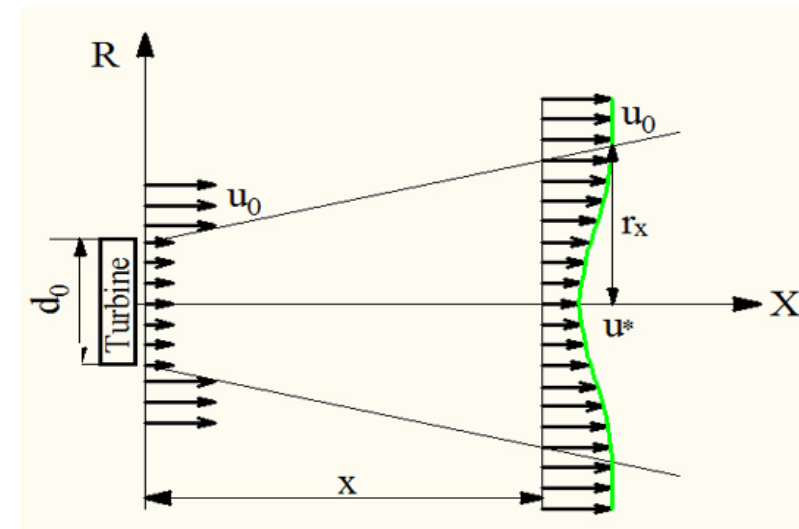
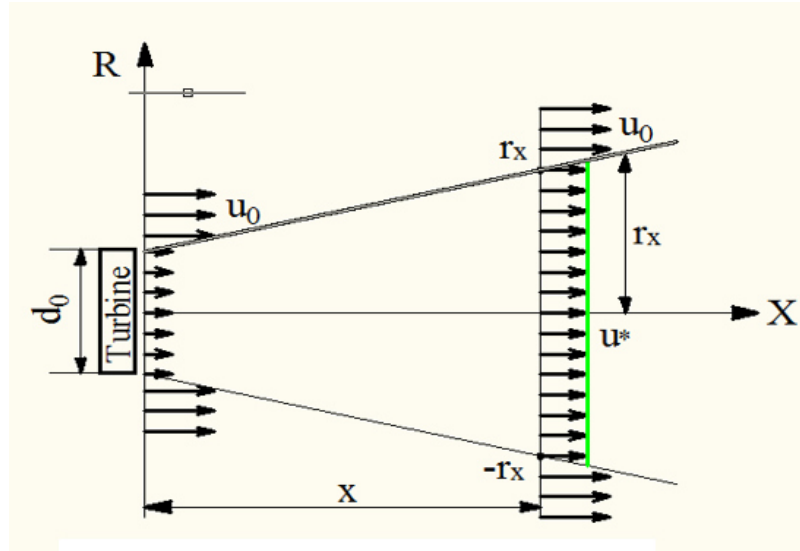
Optimized Layout and Wind Turbine Power
(with Decommissioning Strategy)

Results of Optimized Layouts

	Convention strategy	Decommissioning strategy	
Number of wind turbine	40	40	
Service years	2×20	40	
Energy yield (Gw·h)	2×7.55×10 ³	13.18×10 ³	
Total cost (MHKD)	2×8.96×10 ³	13.47×10 ³	24.83%
COE (HKD/Kw·h)	1.19	1.02	13.94%



Study on wind turbine wake model



Jenson:
$$\frac{\Delta u}{u_0} = (1 - \sqrt{1 - C_T}) / \left(1 + \frac{2kx}{d_0}\right)^2$$

Jenson-Gaussian:
$$u = A \left(\frac{1}{\sigma \sqrt{2\pi}} \cdot e^{\frac{-r^2}{2\sigma^2}} \right) + B$$

Three assumptions:

1. The same radius: $2.58\sigma = r_x$
2. When $r=r_x$: $A \left(\frac{1}{\sigma \sqrt{2\pi}} \cdot e^{\frac{-(\pm r_x)^2}{2\sigma^2}} \right) + B = u_0$
3. The same mass flux: $\int_{-r_x}^{r_x} \left(A \left(\frac{1}{\sigma \sqrt{2\pi}} \cdot e^{\frac{-(y)^2}{2\sigma^2}} \right) + B \right) dx = u^* \cdot 2r_x$



$$\begin{cases} u^* = u_0 \left[1 - 2a / \left(1 + kx / r_1\right)^2 \right] \\ u = u_0 - (u_0 - u^*) \frac{5.16}{\sqrt{2\pi}} \cdot e^{\frac{-r^2}{2 \left(\frac{r_x}{2.58}\right)^2}} \end{cases}$$



Turbine wake model development

Improved Wake Model: new development

Wake decay constant k was effected by ambient turbulence level o that the turbine induces turbulence!

Before modified k , turbulence model should be improved.

Frandsen et al's model, 1996

$$I_{wake} = \sqrt{K_n \frac{C_T}{(x/D)^2} + I_0^2}$$

Tian et al.'s model, 2015

$$I_{wake} = K_n \frac{C_T}{x/D} + I_0$$

Iwake is determined by the I_0 , C_T and x/D .

Proposed turbulence model:

$$I_{wake} = \left(K_n \frac{C_T}{(x/D)^{0.5}} + I_0^{0.5} \right)^2$$



Turbine wake model development

Improved Jenson-Gaussian Wake Model: Development

Using this equation to calculate k_{wake} :
$$k_{wake} = k \frac{I_{wake}}{I_0}$$

Replacing wake decay constant k in the Jenson-Gaussian wake model using k_{wake}

Improved Jenson-Gaussian wake model:

$$\begin{cases} u^* = u_0 \left[1 - 2a / \left(1 + k_{wake} x / r_1 \right)^2 \right] \\ u = u_0 - (u_0 - u^*) \frac{5.16}{\sqrt{2\pi}} \cdot e^{-\frac{r^2}{2 \left(\frac{r_x}{2.58} \right)^2}} \end{cases}$$

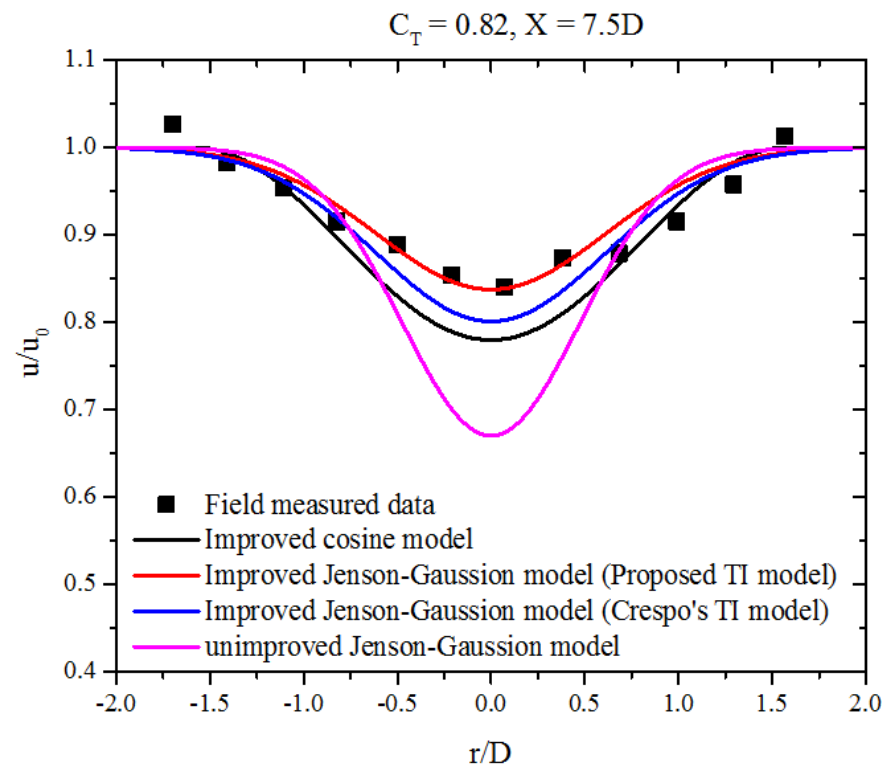
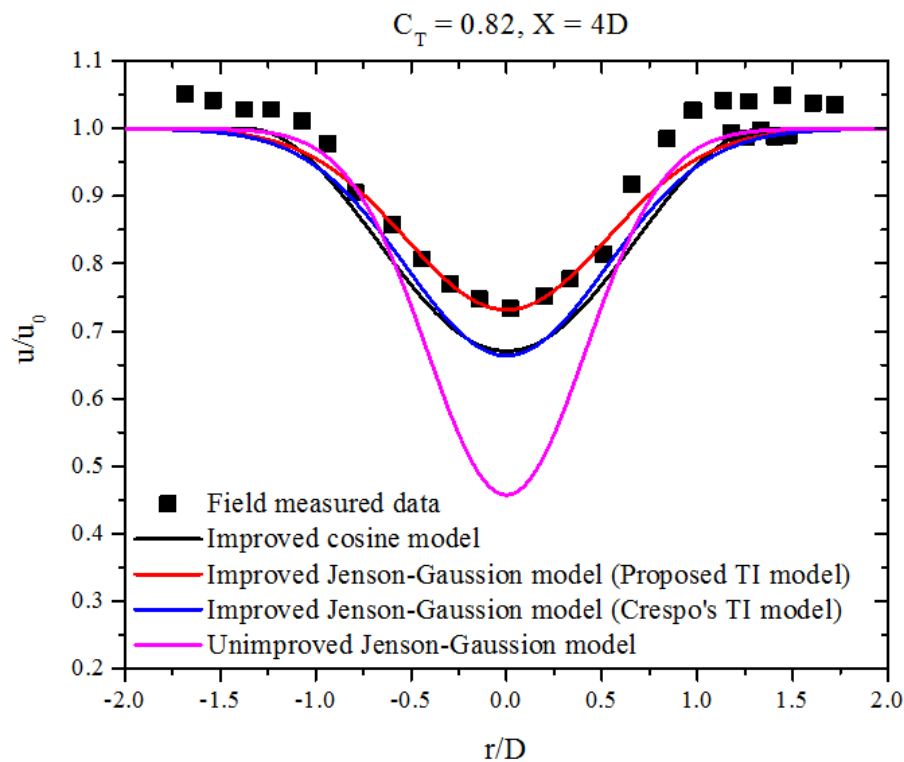


Turbine wake model development

Improved Jensen-Gaussian Wake Model: Validation

With previous models and data from field experiment (Taylor's study of Nibe site).

Two turbines, 45m hub height, 40 diameters, wind speed of 8.55m/s.



'Qualified' good performance is obtained by the improved Jensen-Gaussian wake model !



Turbine wake model development

Analytical Wake Model for Multiple Turbines in Row: superposition

Wake model of single turbine:

$$\begin{cases} u^* = u_0 \left[1 - 2a / (1 + k_{wake} x / r_1)^2 \right] \\ u = u_0 - b \cdot \exp\left[\frac{-(r - r_c)^2}{2s_w^2} \right] \end{cases}$$

$$\begin{aligned} b &= (u_0 - u^*) \frac{5.16}{\sqrt{2\pi}} \\ s_w &= r_x / 2.58 \end{aligned}$$

Wake model of two turbines:

$$\begin{cases} u^* = u_0 \left[1 - 2a / (1 + k_{wake} x / r_1)^2 \right] \\ u = u_0 - b_1 \left\{ \exp\left[\frac{-(r - r_{c1})^2}{2s_{w1}^2} \right] \right\} - b_2 \left\{ \exp\left[\frac{-(r - r_{c2})^2}{2s_{w2}^2} \right] \right\} \end{cases}$$

Wake model of multiple turbines:

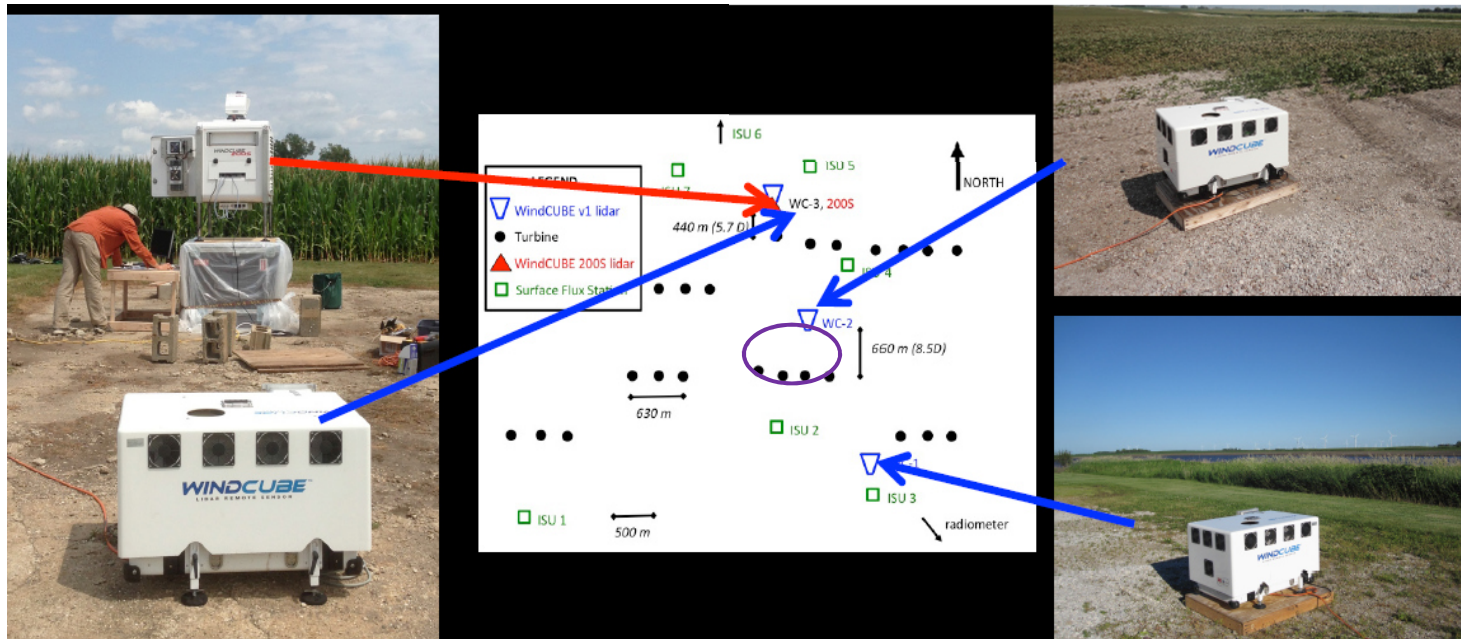
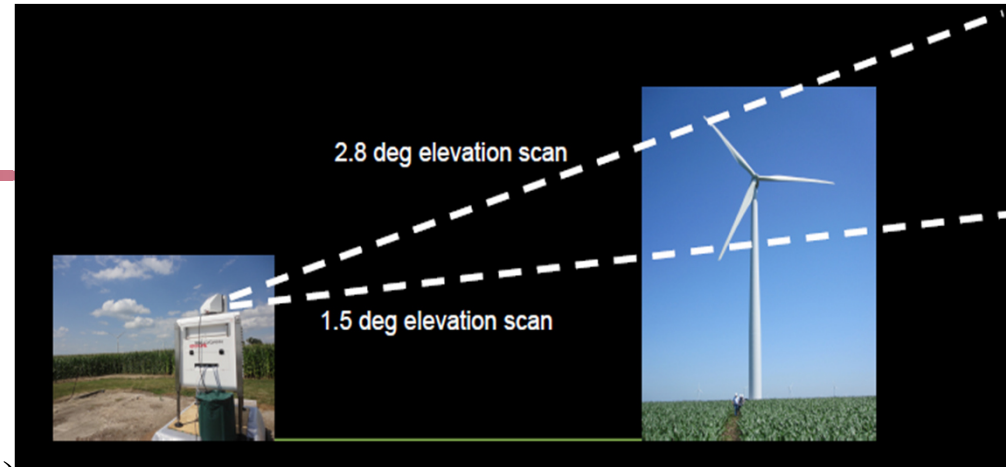
$$\begin{cases} u^* = u_0 \left[1 - 2a / (1 + k_{wake} x / r_1)^2 \right] \\ u = u_0 - b_1 \left\{ \exp\left[\frac{-(r - r_{c1})^2}{2s_{w1}^2} \right] \right\} - \dots - b_n \left\{ \exp\left[\frac{-(r - r_{cn})^2}{2s_{wn}^2} \right] \right\} \end{cases}$$



Field experiment

CWEX-13 Field Experiment:

- 300 MW of GE 1.5 XLE
(80m hub height, 80m D)
- Three profiling lidars (WindCUBEv1)
 - **WS and WD** at 1 Hz; 40m to 220m above the surface; 29 June – 5 Sept, 2013
- One scanning lidar (WindCUBE 200S)
 - Line-of-sight (LOS) velocities from six elevations of PPI scans





Field experiment & findings

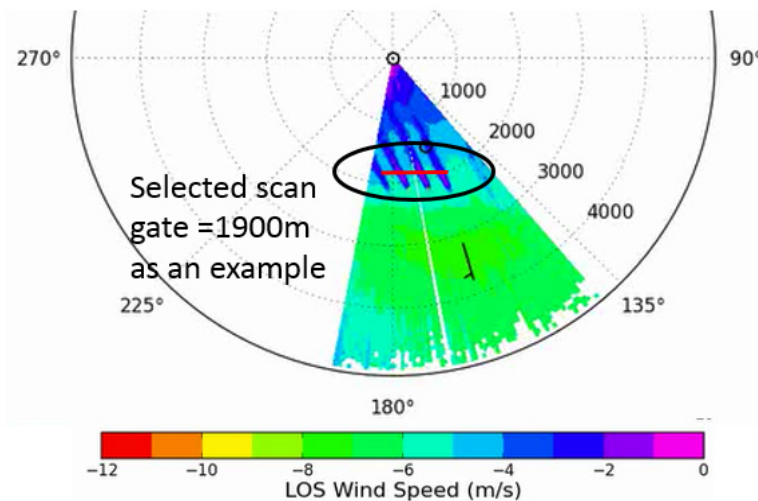
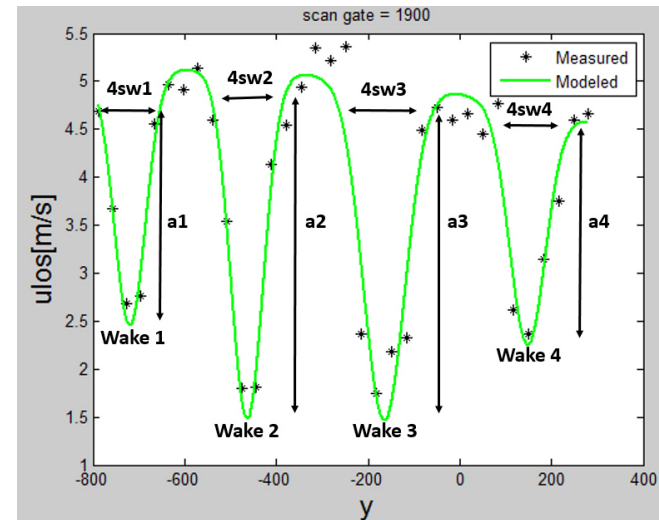
Validation for the Multiple Wakes of Turbines in Row

Fitting and Validation

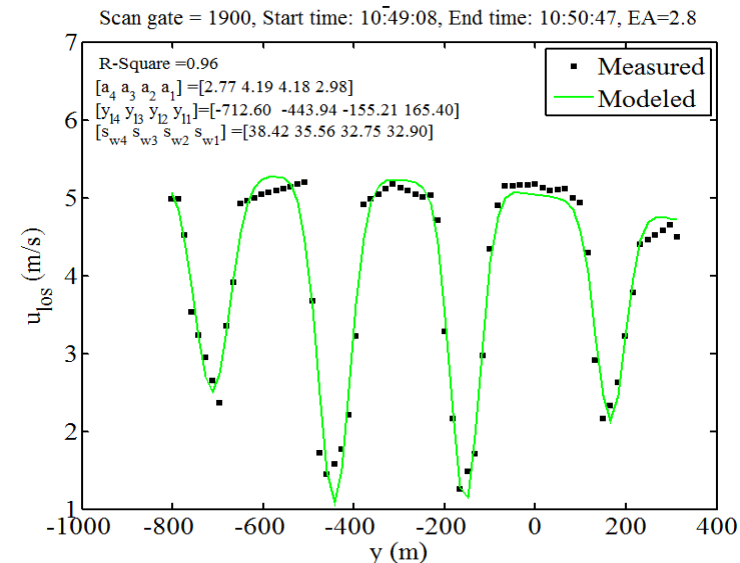
Outer Inner Inner Outer
Divided wind turbine into two styles

Velocity deficit: $VD = \frac{u - (u - a)}{u} \times 100\% = \frac{a}{u} \times 100\%$

Wake width: $w = 4s_w$



2013-08-23-10:49:08 UTC at elevation = 2.8 degrees

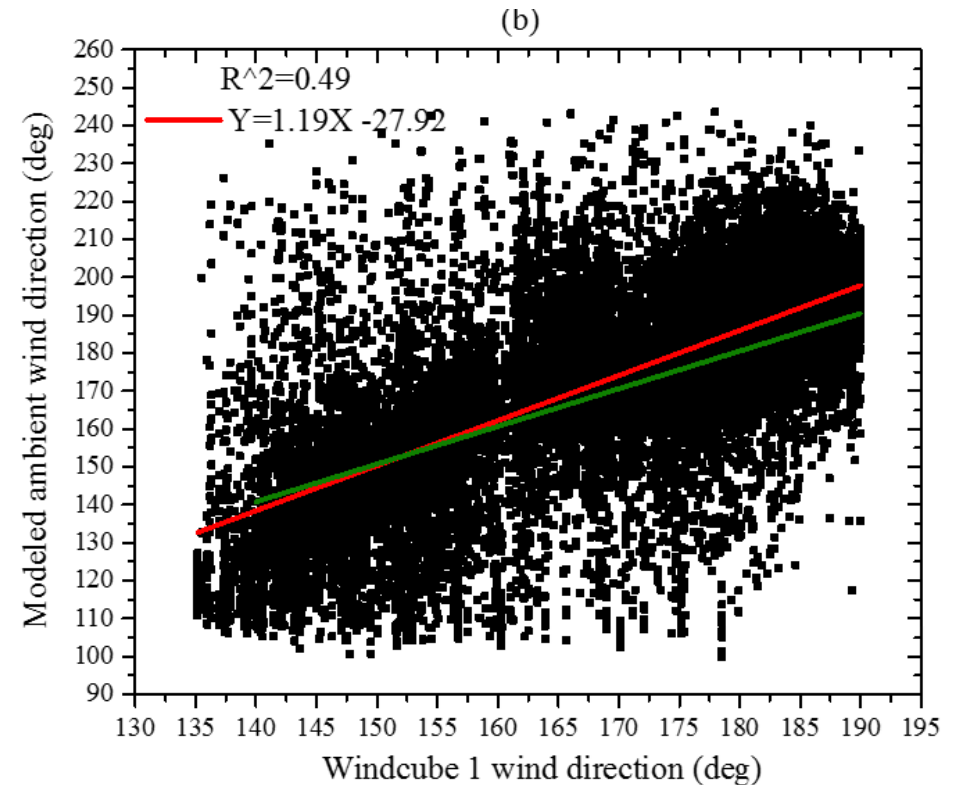
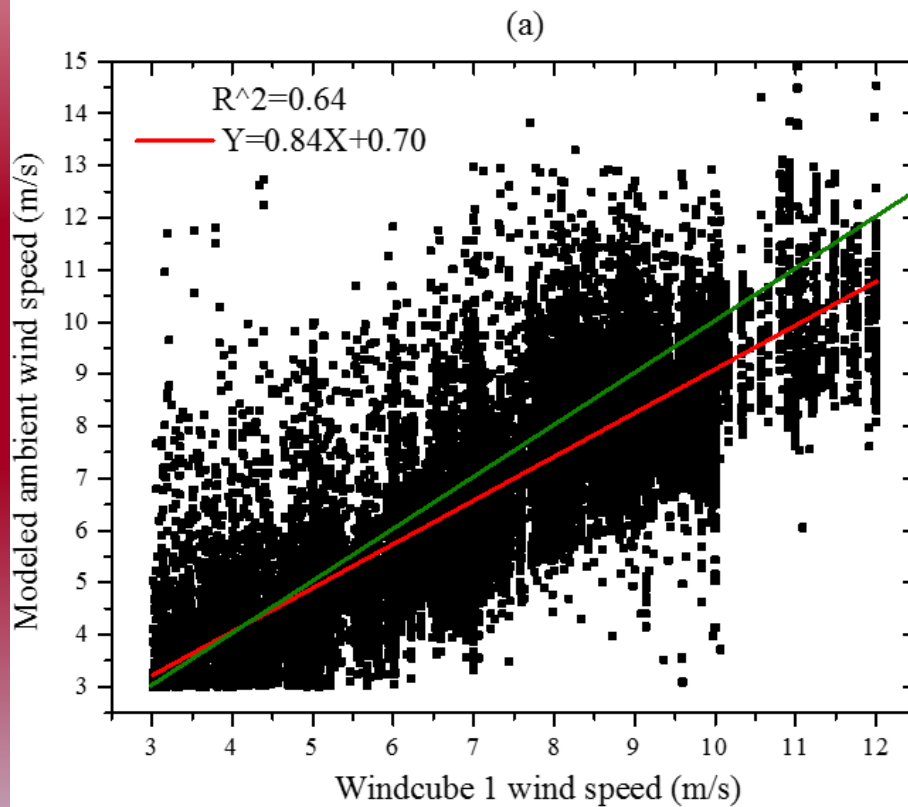




Field experiment & findings

Multiple Wakes' Characteristics under Different Atmospheric Conditions

Comparisons between measured data and modeled

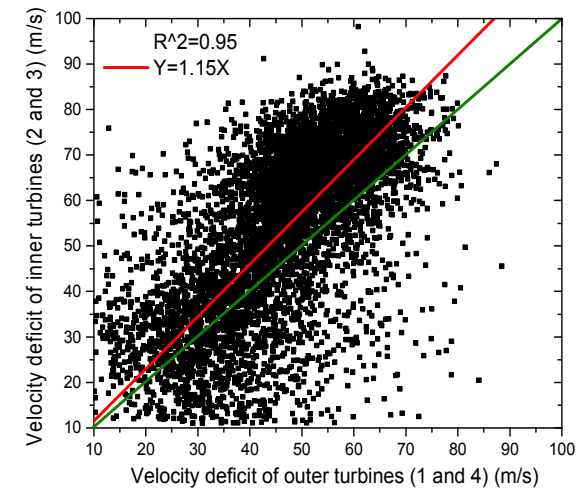
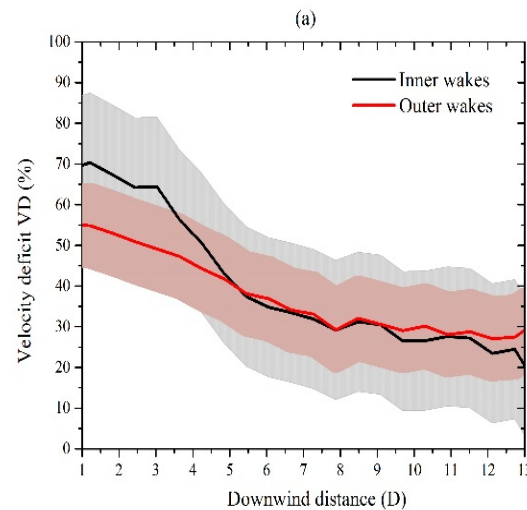
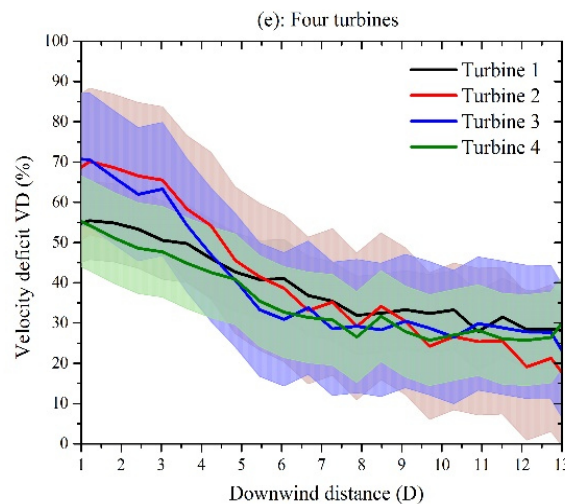




Field experiment & findings

Multiple Wakes' Characteristics under Different (ACs)

- Velocity deficit



Summarizes:

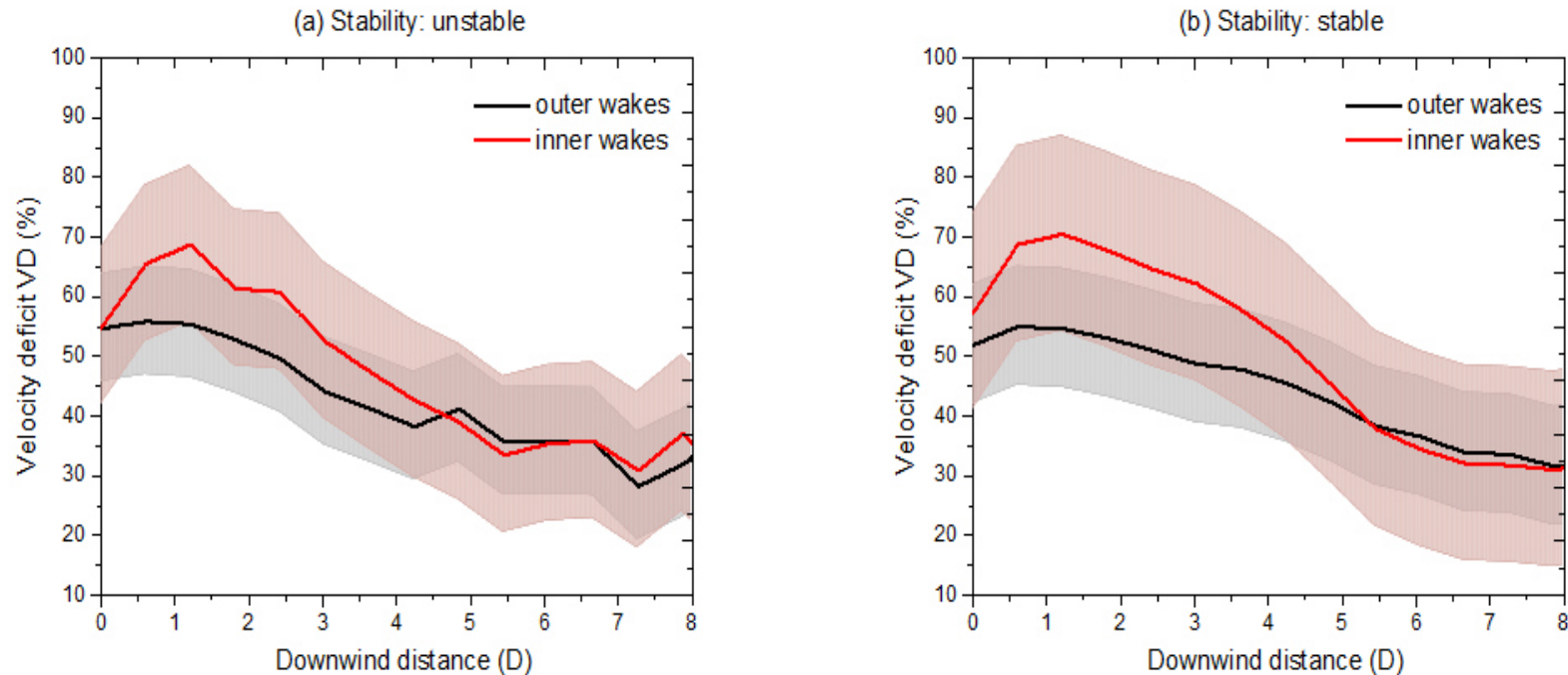
- Velocity deficit, **55%** for outer turbine and **70%** for inner ones.
- No differences after the downwind distance of **5D**.
- The VD of the inner one is **1.15-fold** of VD caused by the outer turbine.
- Wakes from the outer turbines **erode faster** than that from the inner ones.



Field experiment & findings

Multiple Wakes' Characteristics under Different ACs

- Velocity deficit under different atmospheric stabilities



Summarizes:

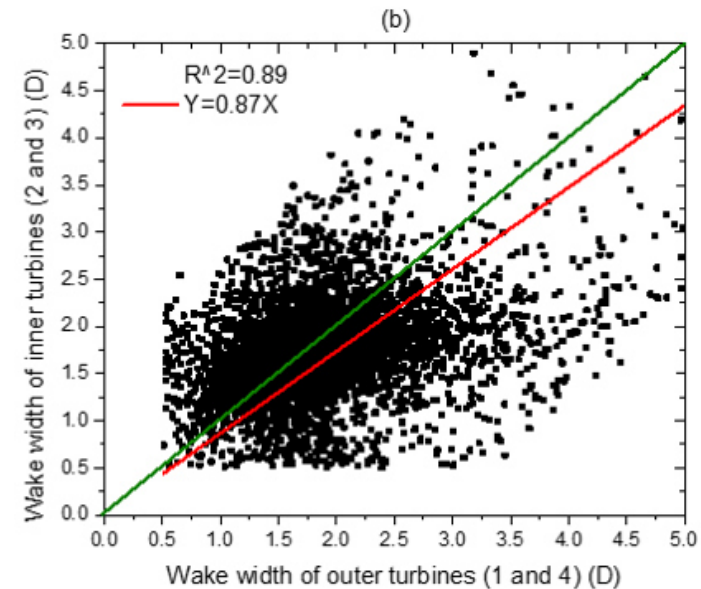
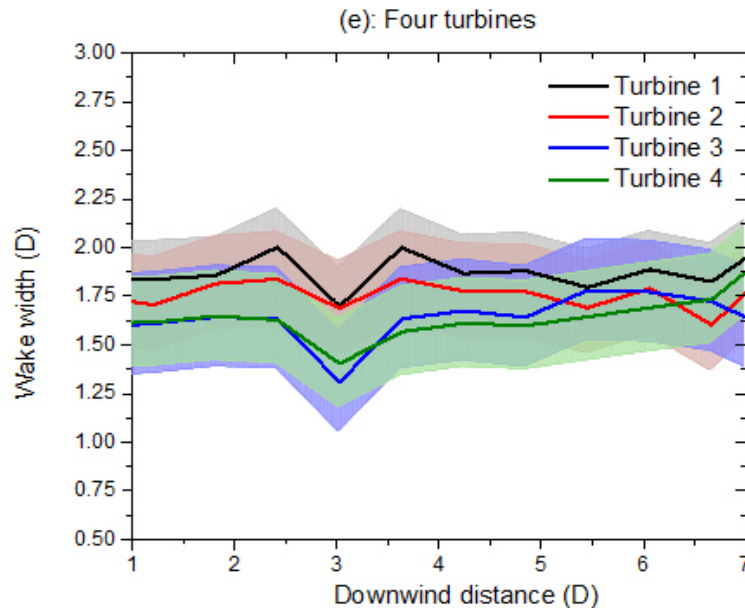
Few influence of the atmospheric stabilities on the velocity deficit can be observed. Still the inner wakes have **bigger velocity deficit** than that of the outer wakes in both stable and unstable conditions.



4. Field experiment & findings

Multiple Wakes' Characteristics under Different ACs

- Wake width



Summarizes:

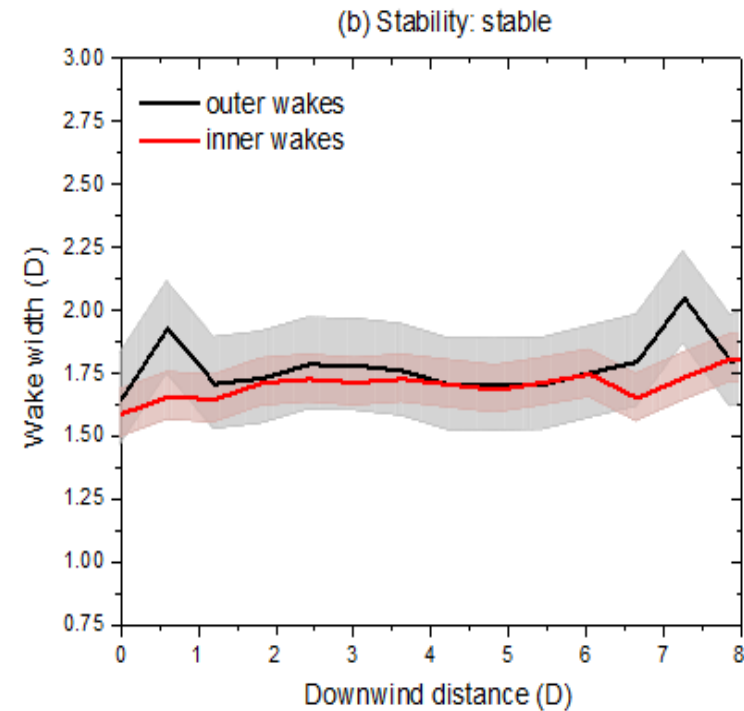
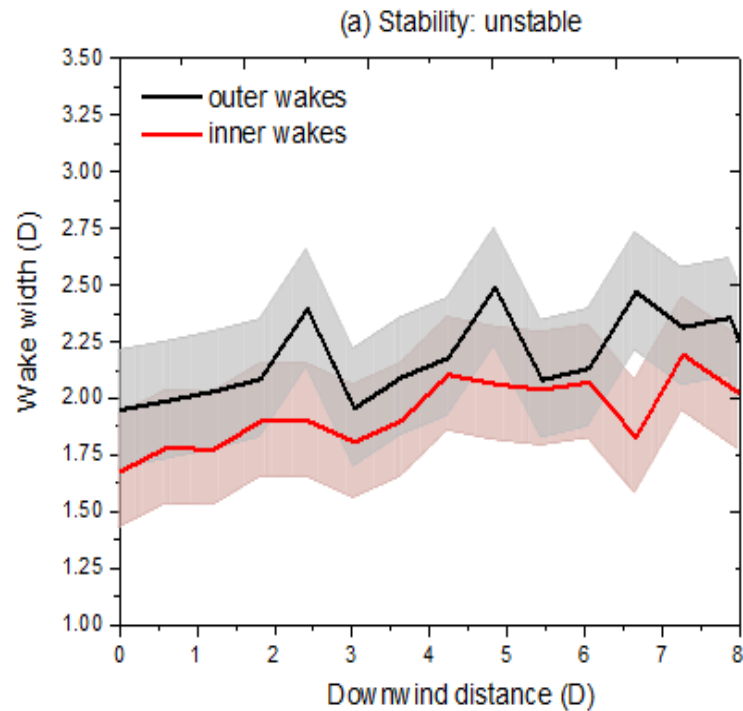
- Wake width, in the range of **1.5D-2.0D**.
- The WW of the inner one is **0.87-fold** of WW caused by the outer turbine.



4. Field experiment & findings

Multiple Wakes' Characteristics under Different ACs

- Wake width under different atmospheric stability



Summarizes:

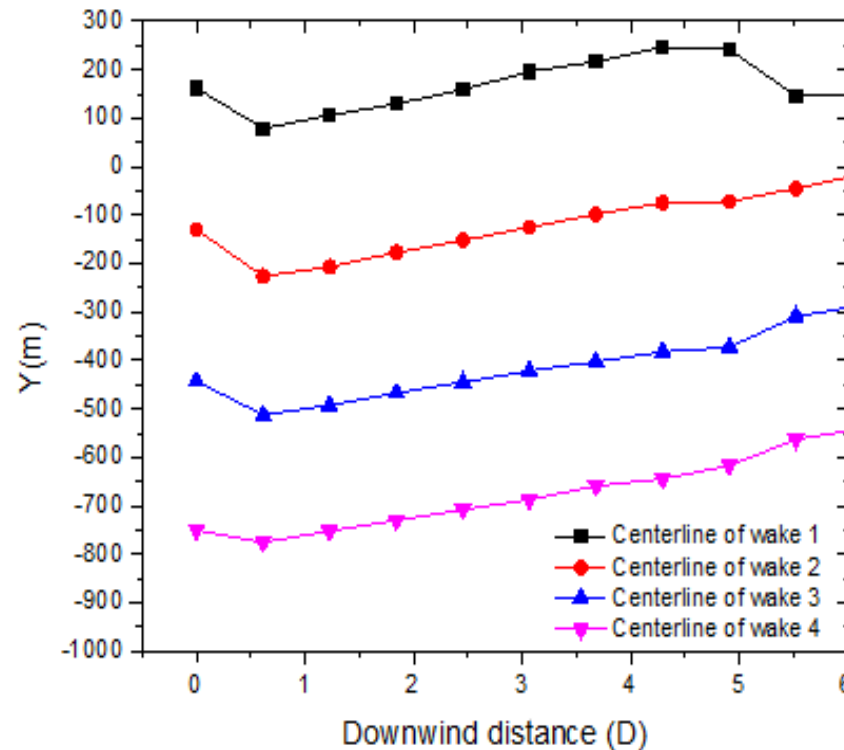
The outer wakes expand more than the inner wakes under unstable atmospheric conditions while there is no significant difference between the widths under stable conditions.



4. Field experiment & findings

Multiple Wakes' Characteristics under Different ACs

- Wake centerline



Summarizes:

Night on August 23 from 10:26:00 to 12:09:33 UTC, the wind direction was in the range 153° - 160° . **The centerlines have the same trend after the row of turbines.**



Study on wind turbine layout optimization

1. Basic Models for the Optimization Program Development

Optimal layout pattern can increase power generation and reduce COE.

Wake model:
$$u_i = u_0 \times [1 - \sqrt{\sum_{j=1}^N (1 - u_j / u_0)^2}]$$

Power generation:
$$P = C_p(\lambda, \beta) \rho A u^3 / 2$$

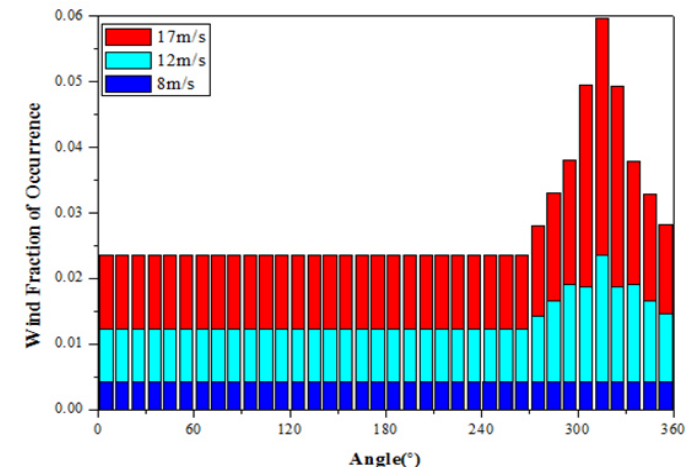
Cost model:
$$\text{COST} = N \times [\frac{2}{3} + \frac{1}{2} e^{-0.00174 N^2}]$$

Wind farm efficiency:
$$\eta_{WF} = \sum_{i=1}^N 0.3 \times u_i^3 / N \times (0.3 \times u_0^3)$$

Wind farm site	
square region:	2km*2km
The ground roughness z_0	0.3m
Wind turbine properties	
Hub height	60m
Rotor radius	40m
Thrust coefficient	0.88

Wind Conditions:

Case NO.	Case description	Wind speed(m/s)	Wind Direction
1	Constant Wind Speed; Fixed Wind Direction	12	Fixed 0°
2	Constant Wind Speed; Variable Wind Direction	12	equal probability 0-360°
3	Variable Wind Direction; Variable Wind Direction	8,12,17	Seen from the following Figure

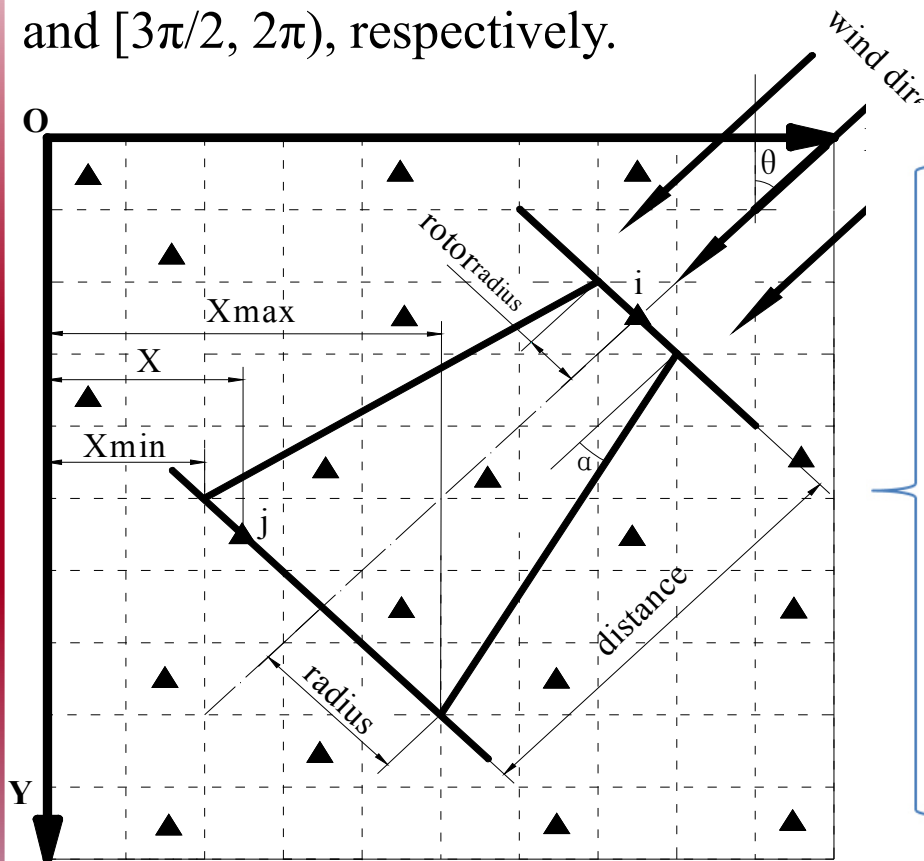




5. Turbine layout optimization program development

2. Velocity calculation based on wake effect

Calculate the velocity deficit when the WD in the range of $[0, \pi/2)$, $[\pi/2, \pi)$, $[\pi, 3\pi/2)$ and $[3\pi/2, 2\pi)$, respectively.



$$\text{distance} = \frac{|\tan(\pi - \theta) * x - y + y_i - \tan(\pi - \theta) * x_i|}{\sqrt{(\tan(\pi - \theta))^2 + 1}}$$

$$\text{radius} = \text{rotor}_{\text{radius}} + \alpha * \text{distance}$$

$$X_{\text{min}} = x_i - \text{distance} * \cos\left(\frac{\pi}{2} - \theta\right) - \text{radius} * \sin\theta$$

$$X_{\text{max}} = x_i - \text{distance} * \cos\left(\frac{\pi}{2} - \theta\right) + \text{radius} * \sin\theta$$

$$u_j^i = u_0 * \frac{2a * r_d^2}{(r_d + \alpha x)^2} = u_i * \frac{2a * \text{rotor}_{\text{radius}}^2}{(\text{rotor}_{\text{radius}} + \alpha * \text{distance})^2}$$

$$= u_i * \frac{2a * \text{rotor}_{\text{radius}}^2}{\left(\text{rotor}_{\text{radius}} + \alpha * \left(\frac{|\tan(\pi - \theta) * x - y + y_i - \tan(\pi - \theta) * x_i|}{\sqrt{(\tan(\pi - \theta))^2 + 1}}\right)\right)^2}$$

$$u_j = u_0 - \sum_{i=1}^N u_j^i$$

Two steps: 1. Check wake number and 2, calculate velocity

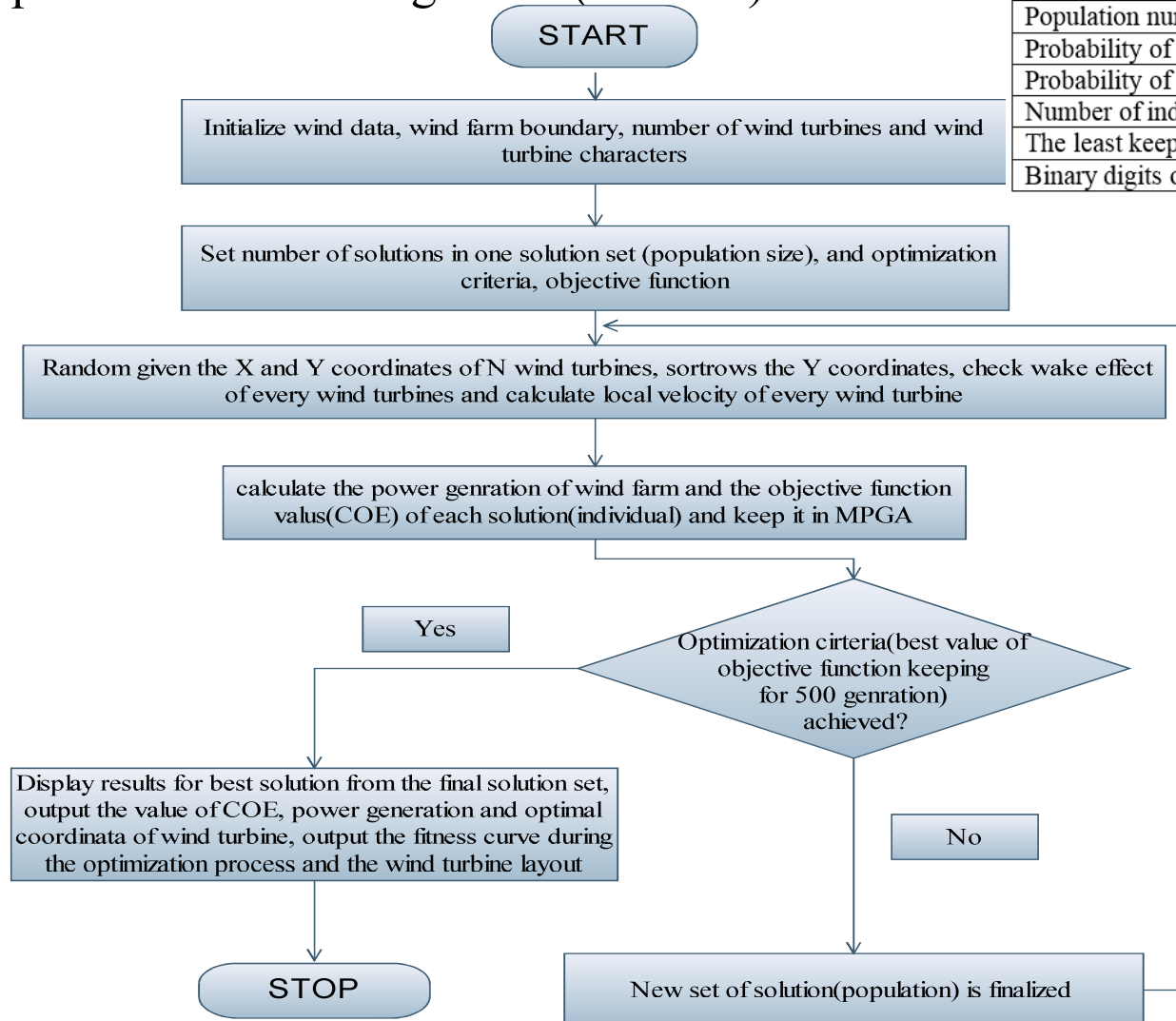


5. Turbine layout optimization program development

3. Program design

Multiple Population Genetic Algorithm(MPGA) is used

Parameters	Value
Population number	10
Probability of crossover	0.7-0.9
Probability of mutation	0.001-0.05
Number of individual	40
The least keeping generations	500
Binary digits of variable	20





6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6. Three layout patterns: Scattered, aligned and staggered

- From the **aspect of engineering**, turbines are recommended to be installed in arrays.
- **7D -12D** in prevailing wind direction (**PWD**) and **5D-10D** in crosswind direction (**CWD**) (Huang et al. 2012).
- **No recommendations** about Hong Kong offshore.



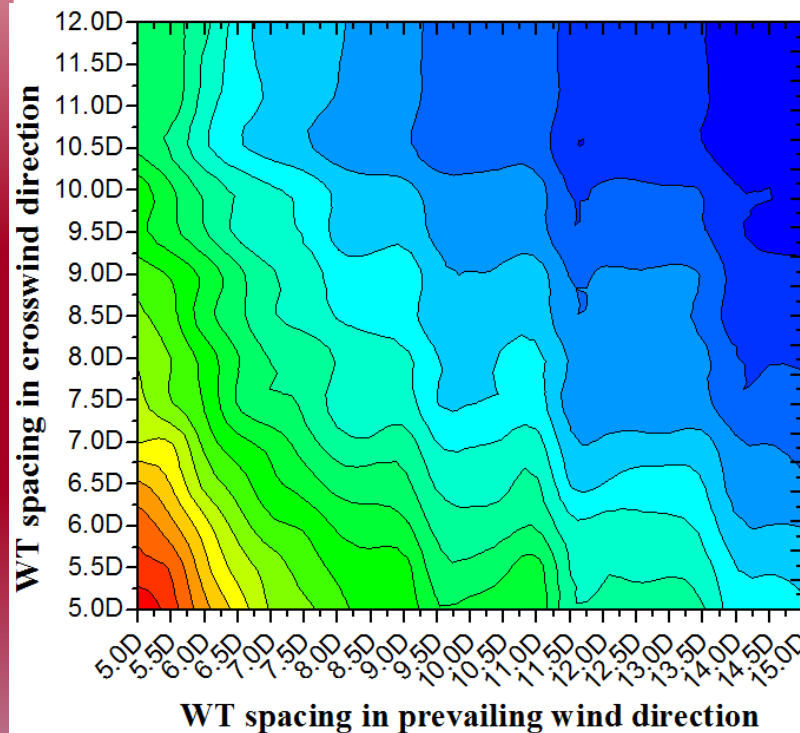
North Carolina offshore wind farm



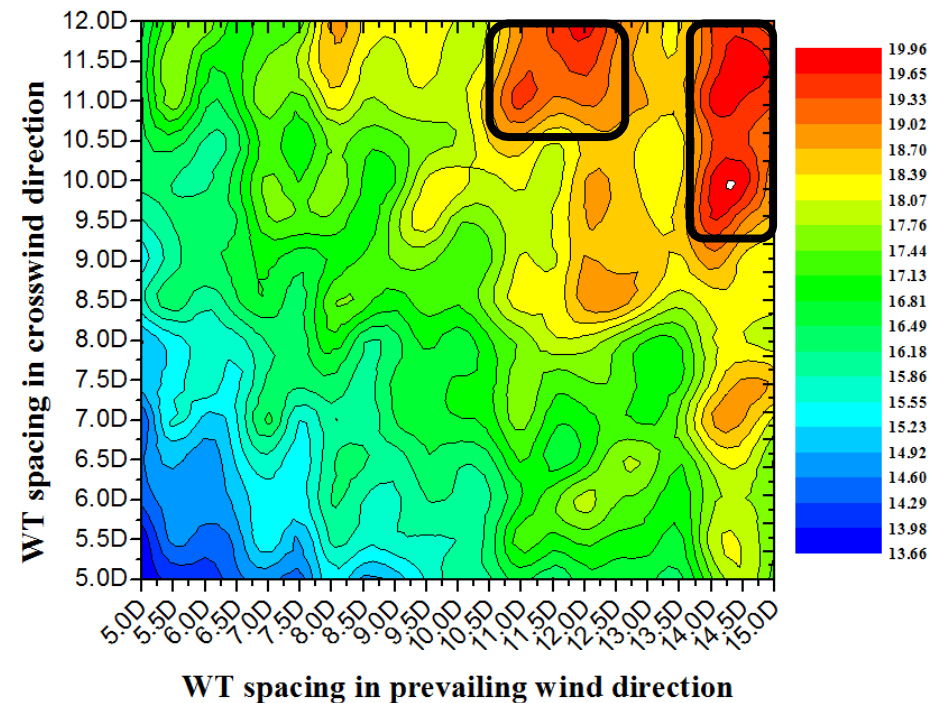
6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6. Results for Aligned and Staggered WF Configurations

6.1 Energy Generation : **Aligned**



AEG ($\times 10^8$ kWh)



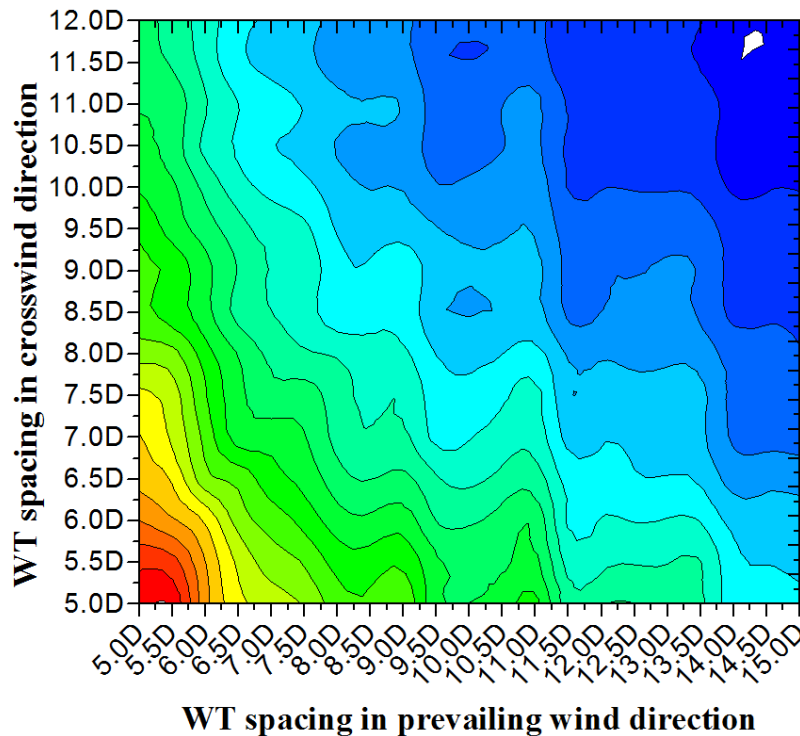
AEG per Turbine ($\times 10^6$ kWh)



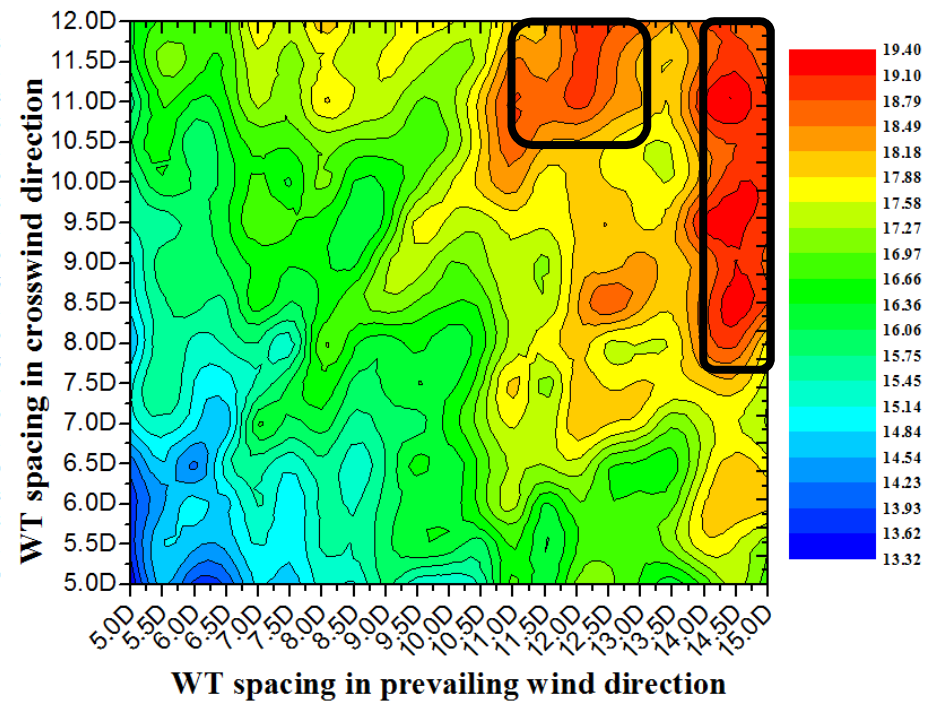
6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6. Results for Aligned and Staggered WF Configurations

6.3 Energy Generation : **Staggered**



AEG ($\times 10^8$ kWh)



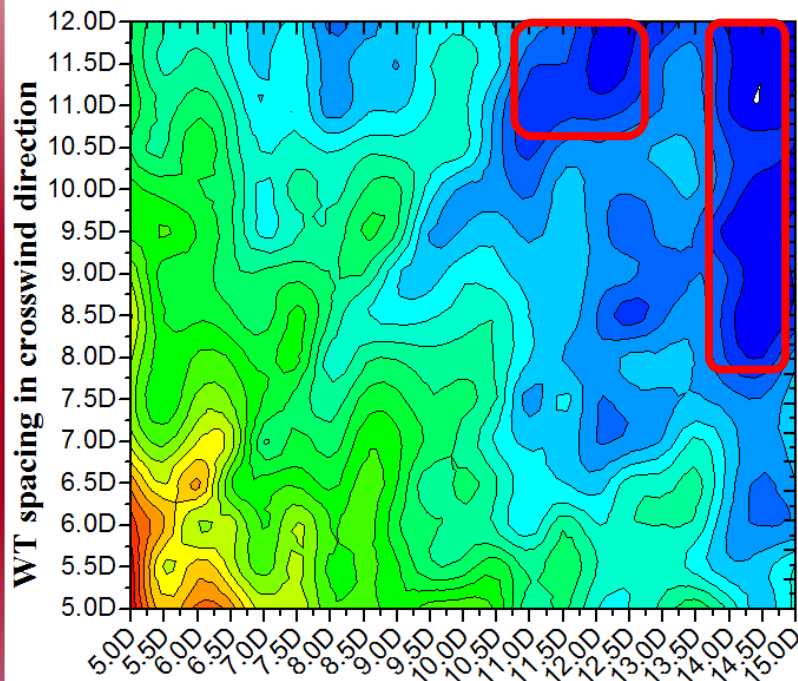
AEG per Turbine ($\times 10^6$ kWh)



6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6. Results for Aligned and Staggered WF Configurations

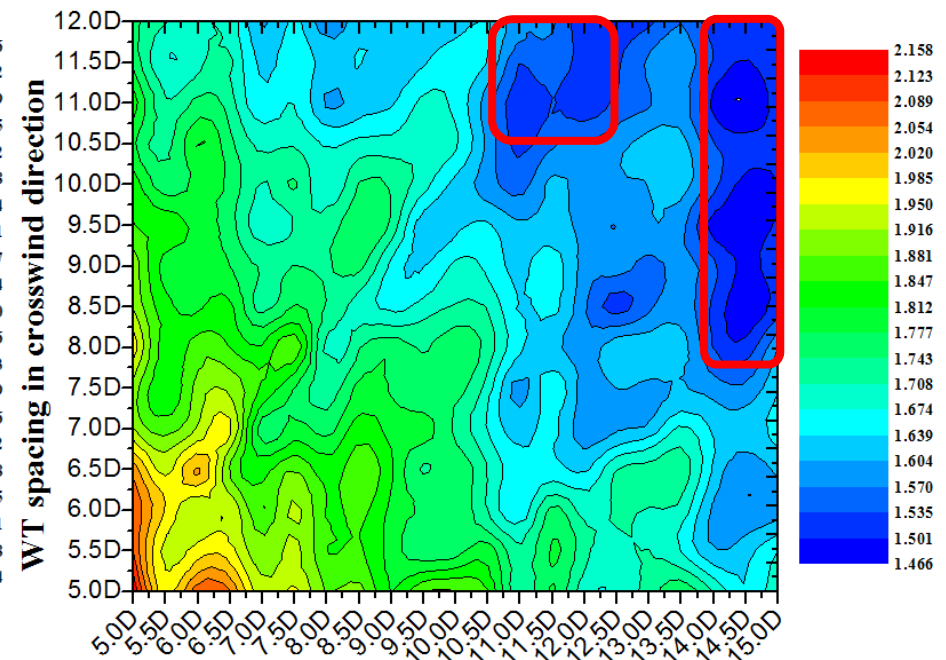
6.4 Results of COE



WT spacing in prevailing wind direction

Aligned (HKD/kWh)

1.5-2.1 HKD/kWh



WT spacing in prevailing wind direction

Staggered (HKD/kWh)

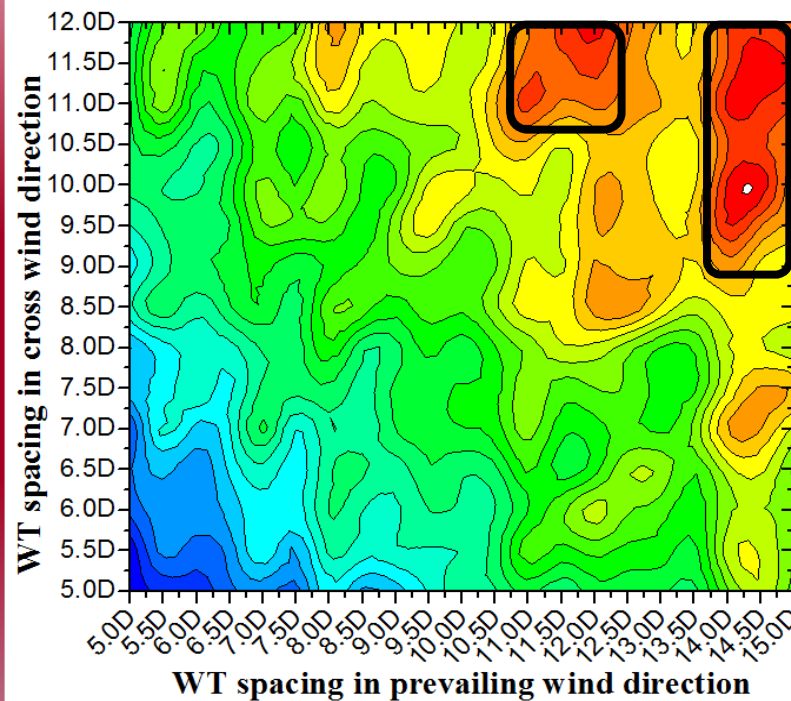
1.5-2.2 HKD/kWh



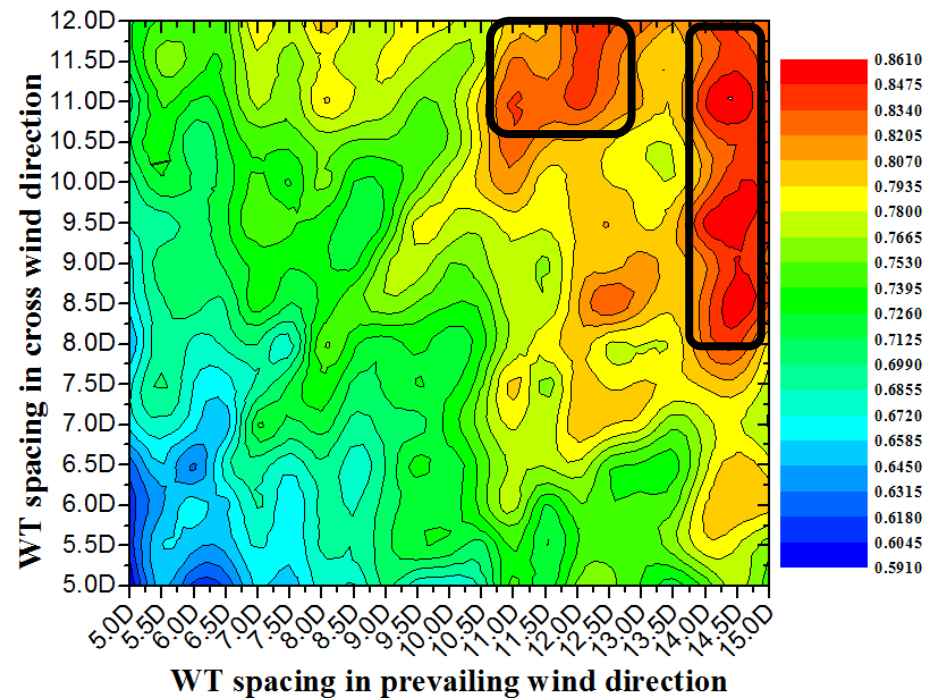
6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6. Results for Aligned and Staggered WF Configurations

6.5 Results of Wind farm efficiency



Aligned (HKD/KWh)

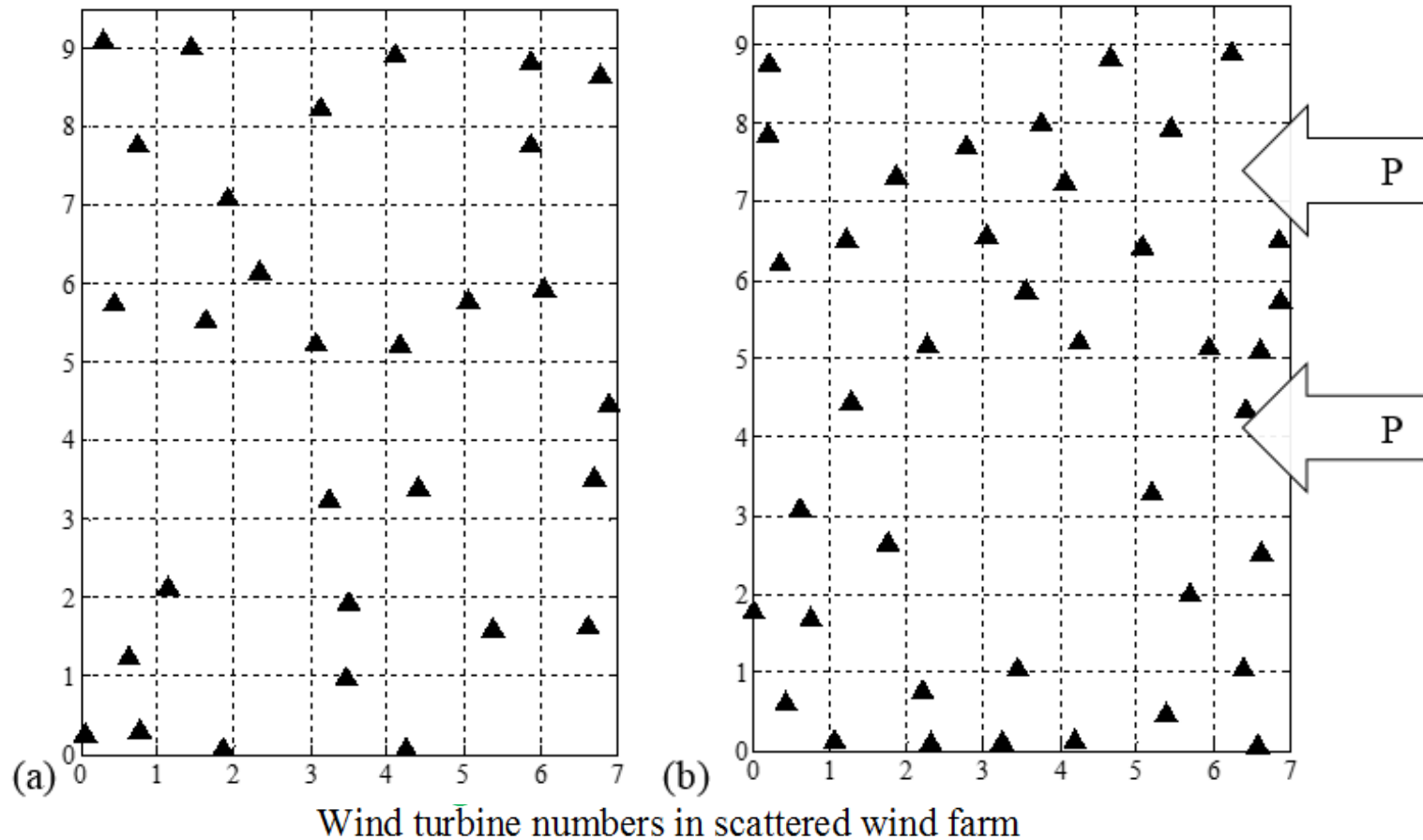


Staggered (HKD/KWh)



6. Determination of the optimal layout pattern and power potential in Hong Kong offshore

6.6 Optimal Turbine Number for Scattered WF Configurations





Conclusions

- Wind power develops fast and offshore wind power can provide meaningful power supply to coastal urban areas for renewable energy applications.
- The annual offshore wind power generation could be 40.8×10^8 kWh in Hong Kong, which accounts for 32.9% of the local annual electricity consumption in 2012.
- The developed 2-dimensional wake model is a new development in this professional area.
- The MPGA optimization program has been successfully developed and validated, which is a useful tool in wind farm micro-siting and power generation prediction.
- Decommissioning costs should be included for life-cycle cost analysis.



Thanks

Q & A